Summary of MASCO Meeting June 18 - 19, 2012

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Program Organization

- Integrated, science based, national level program involving LLNL, ORNL, PNNL, UCLA, UCSB, and UTK.
- International fusion materials programs are coordinated through IEA Implementing Agreements involving Canada (inactive), China, European Union, India, Japan, Korea, Russian Federation, Switzerland and United States.
- The Fusion Materials Sciences Program is involved in strong, wellestablished international collaborative programs:
 - DOE/JAEA (irradiation experiments in HFIR for structural materials development).
 - DOE/MEXT TITAN (irradiation experiments in HFIR and complementary nonirradiation tests using unique U.S. facilities for structural and functional materials development).
 - EU (e.g. PSI, Riso, irradiation experiments in HFR-Petten).

Budget Distribution by Research Topic

- Current budget allocation: ~\$5,000K
- Early Career Award:
 - J. Marion, LLNL
 - \$500K
- Outcome of materials solicitation will be known soon (~2 weeks):
 - \$2,600K
 - New institutions
 - New research topics
 - Reorganization under discussion



Irradiation Experiments
Mechanical Properties
Helium Effects
Alloy Development
Physical Properties
Fabrication & Joining
Theory & Modeling
Other

Budget Distribution by Material System



Impact of He-Rich Environment on Neutron Irradiated Materials

- A unique aspect of the DT fusion environment is substantial production of gaseous transmutants such as He and H.
- Accumulation of He can have major consequences for the integrity of fusion structures such as:
 - Loss of high-temperature creep strength.
 - Increased swelling and irradiation creep at intermediate temperatures.
 - Potential for loss of ductility and fracture toughness at low temperatures.
- TMS appear to be more resistant to He embrittlement, but He can reach and damage grain boundaries. Property changes under prototypical conditions (T, He/dpa, φt, etc.) have not been fully explored.

Schroeder & Batfalsky, 1983



Helium Bubble Size and Number Density at 500°C, 380 appm He/9 dpa

NFA provide radiation damage resistance by promoting vacancy-interstitial recombination & trapping of He.



NFA - What Are NF?

• $10^{23-24}/\text{m}^3$ of 1 to 4 nm $Y_2\text{Ti}_2O_7$ (mostly)

G. R. Odette and D. T. Hoelzer, JOM 62-9 (2010) 84; Yu et al, Act Mat 60-8 (2012) 356



Strategies to Improve Radiation Resistance may Cause Enhanced Tritium Retention

G.D. Tolstolutskaya et al., 12th Int. Conf. on Environmental Degradation of Materials in Nucl. Power System (TMS, 2005), p. 411



Deuterium retention in 18Cr10NiTi steel implanted to $1 \times 10^{16} \text{ cm}^{-2}$ without He (1) and with He to $5 \times 10^{15} \text{ cm}^{-2}$ (2) and $5 \times 10^{16} \text{ cm}^{-2}$ (3)

He-H behavior at bubbles in Tungsten



At larger He bubbles H segregates to the bubble/matrix interface



B.D. Wirth et al, UTK

Joining of Advanced Steels : ODS to RAF

F82H Plate

- Ends cut from previously tested fracture toughness dual notch bend bars of 14YWT-SM6 and welded into slot in F82H plate
- Joining of sample by FSW was successful!
 - Good overall consolidation of 14YWT
 - Good bonding between 14YWT and F82H
 - Voids present at the bottom of the weld - need to refine the process conditions
- PCBN (Polycrystalline Boron Nitride) pin tool did not fracture!

Friction Stir Weld Zone 14YWT-SM6 14YWT-SM6 14YWT-SM6 14YWT-SM6 14YWT-SM6 14YWT-SM6 Specimen Locations 0 0.25L 0.50L L (30 mm)

Specimen at 0.25L location



Z. Feng and D.T. Hoelzer, ORNL

F82H Plate

Materials Engineering & Design Interface: Empirical Data Extrapolation

Empirical Determination of deformation mechanisms of F82H steels as a function of temperature and strain rate.



NH Creep

0.6

0.8

Shear Strength

Experiments & Modeling of Ductility Loss in Steels

