

Development of Si-W Transient Tolerant Plasma Facing Material

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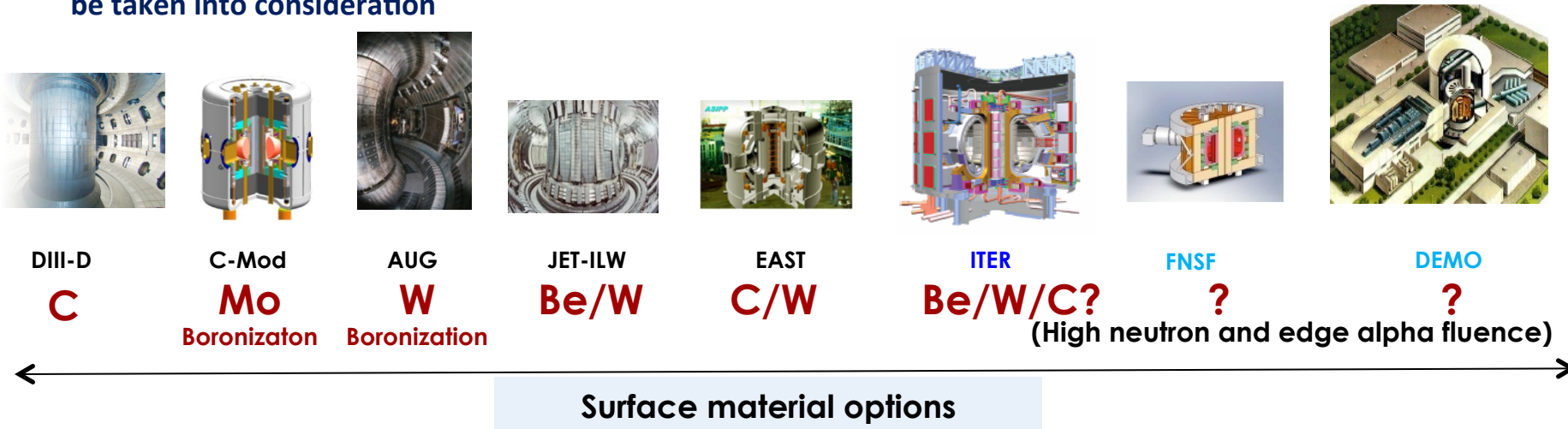


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Surface Material is a Key Item for Fusion Development

Surface material is critically important to next generation tokamak devices:

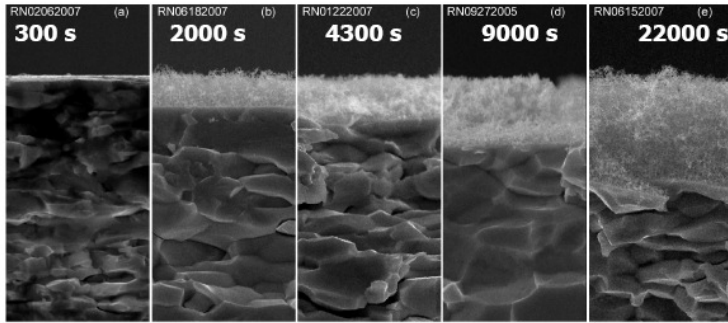
- Plasma performance is affected by transport of impurities
- Surface heat removal, tritium co-deposition and inventory will have impacts on material selection for devices beyond ITER
- Radiation effects from neutrons and edge alphas, material design limits and component lifetimes will have to be taken into consideration



C and Be will not be suitable for the next generation devices and DEMO due to surface erosion and radiation damage. Presently, W is the preferred choice, but feasibility and performance issues have been identified

Significant Issues Projected for W-surface Operation Independent of Alloy Development

SEM cross-sections of W targets exposed to PISCES-B pure He plasmas.



30kV X5,000 5µm UC PISCES
 Consistent He plasma exposures: $T = 1120 \text{ K}$, $\Gamma_{\text{He}^+} = 4\text{--}6 \times 10^{22} \text{ m}^{-2}\text{s}^{-1}$, $E_{\text{ion}} \sim 60 \text{ eV}$
 PISCES

When exposed to He at high temperature, W surface showed growth of W nano-structure from the bottom; the thickness increases with plasma exposure time

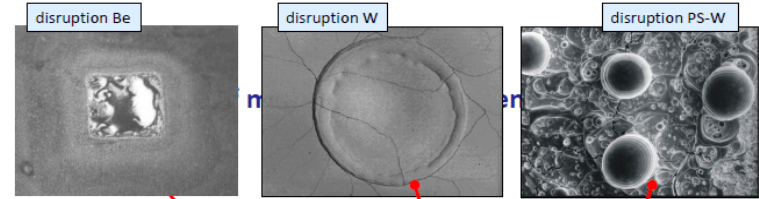
Baldwin and Doerner, Nuclear Fusion 48 (2008) 1-5

Equilibrium thickness of fuzz is expected to form in the erosion zone of a W-divertor, erosion with lower sputter yield than bulk W

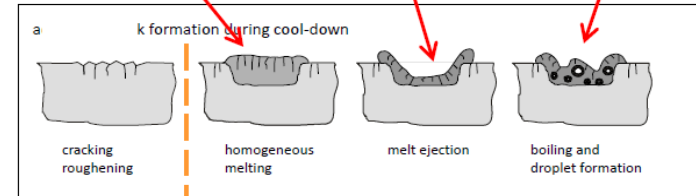
Doerner, UCSD, VLT conf. call Jan. 2011

ITER disruption loading:

10-30 MJ/m² for 0.1 to 3 ms



increasing power density



ELMs | vertical displacement events / plasma disruptions
 melting threshold

Irreversible surface material damage

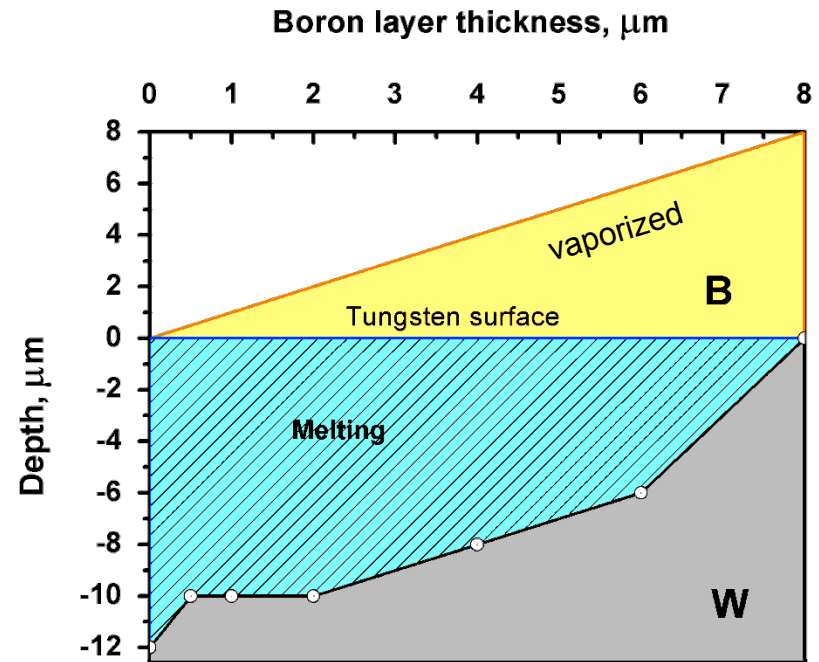
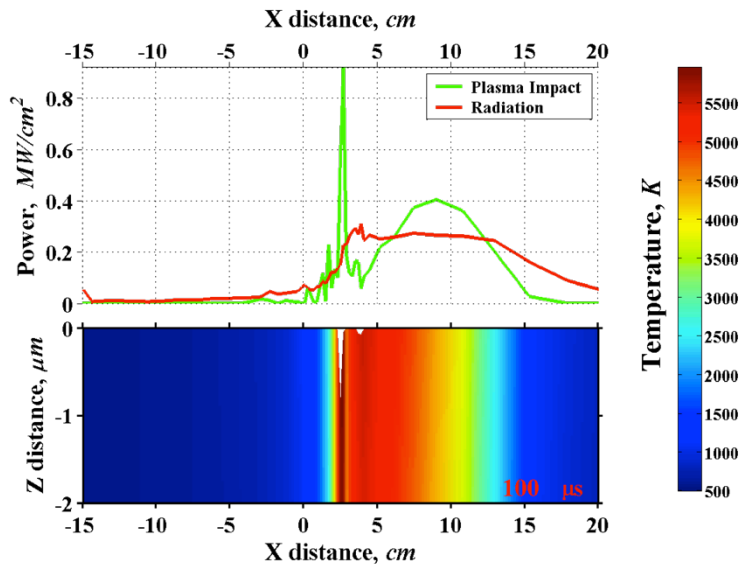
M. Rödiger, Int. HHFC workshop, UCSD Dec. 2009

We cannot eliminate un-predicted disruptions even if disruption detection and mitigation working perfectly

Vapor Shield Effect from Boron Could Protect Substrate W Under Disruptions

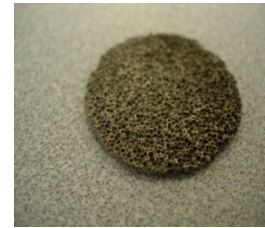
Disruption condition, ITER parameters:

Energy density $E = 25 \text{ MJ/m}^2$
Impact duration $t = 0.1 \text{ ms}$
Magnetic field $B = 5.0 \text{ T}$
Incline angle $\alpha = 5.0 \text{ degree}$

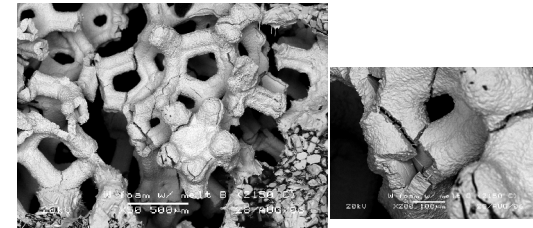


Si W Samples Development History

- 2008 started with W-mesh, sample damaged with melting of B @ $\sim 2000^{\circ}\text{C}$
- 2009 changed from mesh to plate, and DIII-D boronization confirmed B coating thickness of $0.75\ \mu\text{m} < 1\ \mu\text{m}$
- Switched to Si due to much better match in the coefficient of thermal expansion between Si and W
- W disc was destroyed and broken in pieces when trying to fill with molten Si @ $\sim 1400^{\circ}\text{C}$
- 2010: Drilled indentations on W-buttons and the Si was filled in powder form with binder and sintered
- 2010 Si filled W buttons exposed in DIII-D to five plasma discharges
- 2011 obtained new W buttons with indentations and slots
- Sample destroyed and broken in pieces during CVD Si fill mishap @ $\sim 1400^{\circ}\text{C}$
- New CVD filled Si-W buttons exposed to six VDE disruptions & noted the formation of W-silicide eutectic



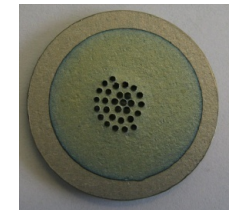
W-mesh



Damaged W-mesh



W-disc



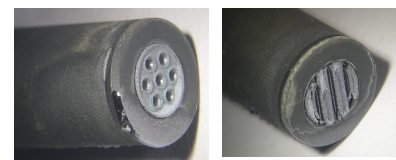
B-coating



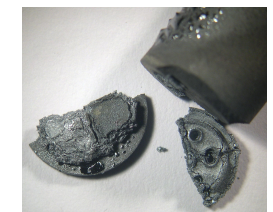
W-buttons



W-buttons with Si



W-buttons in CVD fixture



Broken Si-W-buttons

Exposure to Four LSN Discharges and One Disruption, Surface Si Removed but Minimal Impacts Observed



Si filled W-buttons



Loaded DiMES sample
2 Si-W, 3 graphite, 2 W buttons



W-buttons with
1 mm dia. indentation



Shot 142641-142644

Sample exposed
To 4 LSN discharges



Exposed in
DIII-D lower divertor



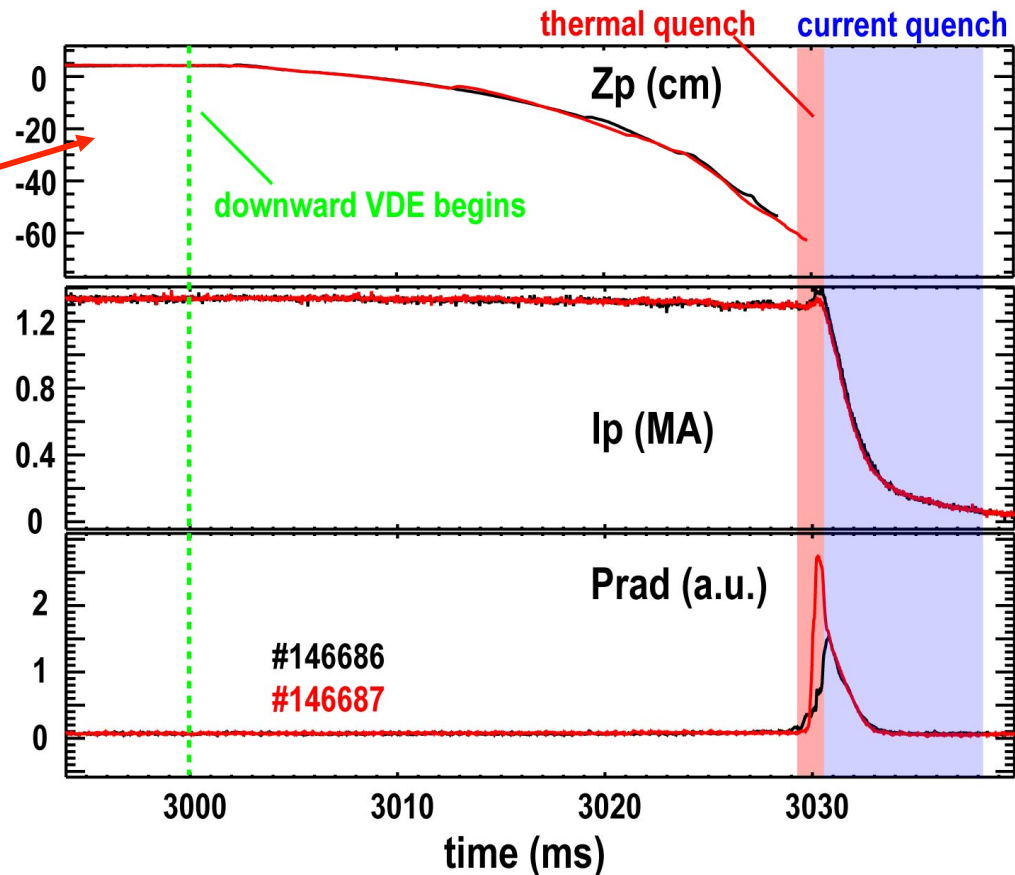
Shot 142706

After one additional disruption
shot without thermal dump on DiMES

Overview of VDE Disruption Experiments

- Create repeatable VDE by turning off feedback and giving plasma slight downward kick with shaping coils
- Achieve reliable exponential growth of vertical position
- Repeat for statistics with 1.5 neutral beam ($W_{th} = 0.7$ MJ) and 4 neutral beam ($W_{th} = 1.1$ MJ) H-mode targets
- Repeat 1.5 neutral beam target and mitigate VDE at various times with neon massive gas injection “MGI” (1200 torr-I)

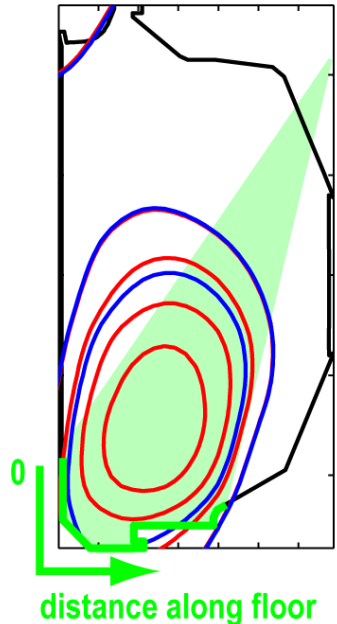
Reliable timing shot of VDEs



Peak Heat Fluxes in VDE Disruption to Lower Inner Wall at Start of CQ

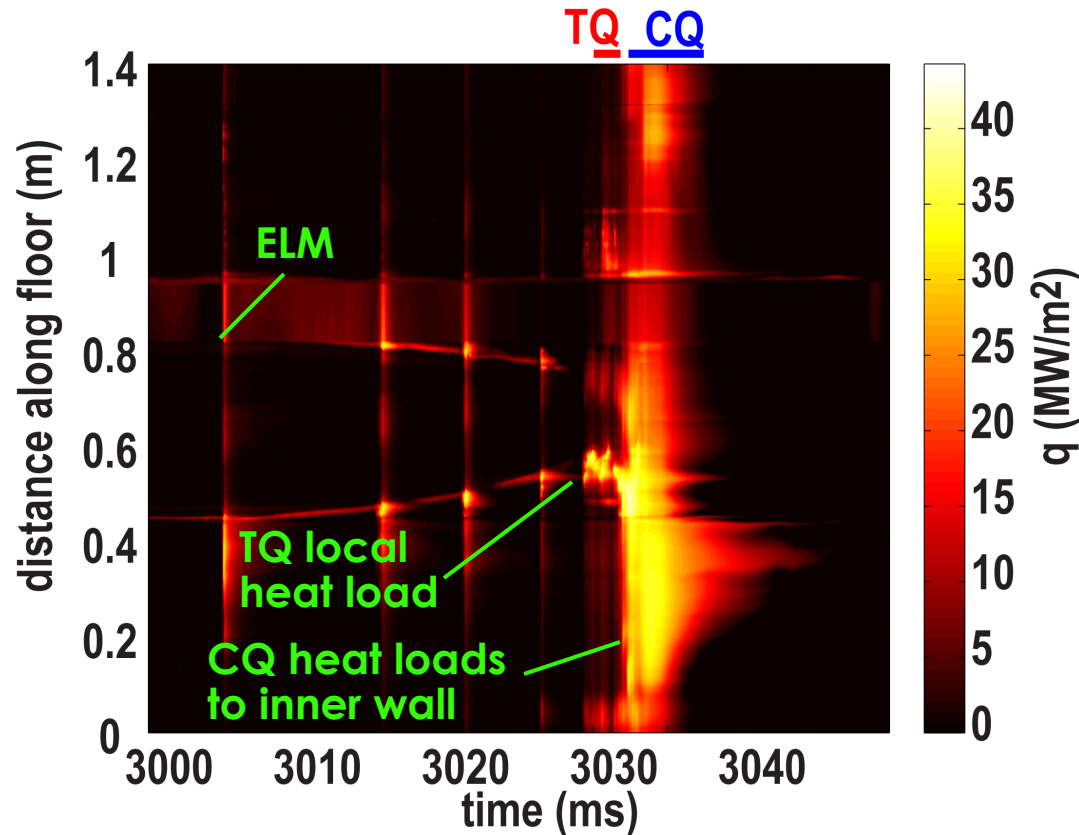
- IR camera run in line-scan mode to achieve high time resolution.
- Heat fluxes to lower divertor can be estimated from changes in IR brightness.
- Peak heat fluxes typically occur not in thermal quench (TQ), but at start of current quench (CQ).

#146688, $t = 3030$ ms



Viewing geometry of IR camera at $R+2$, $\phi = 60^\circ$

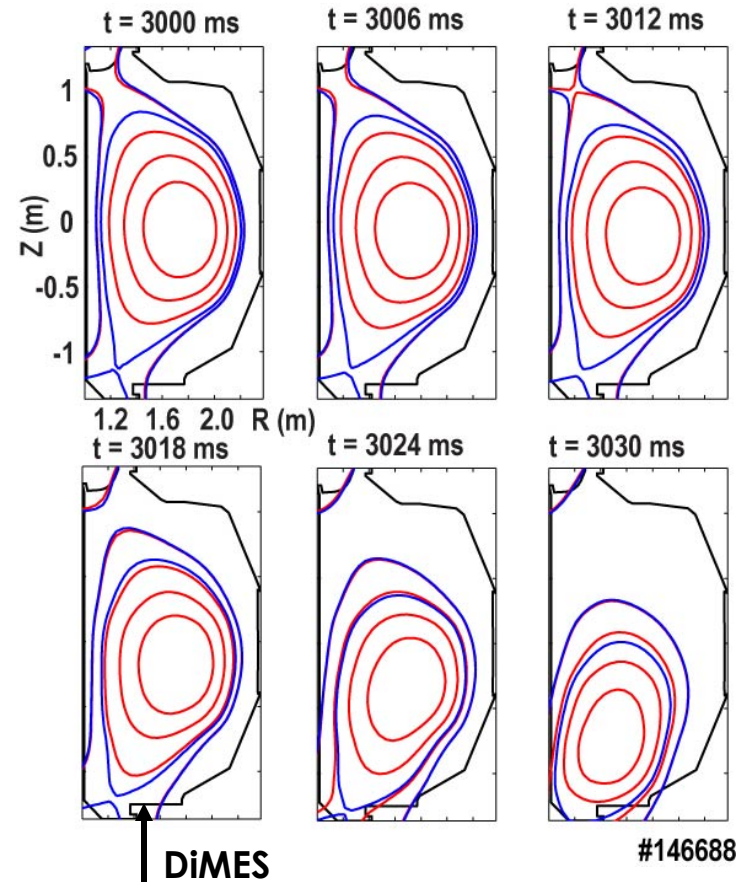
Heat fluxes across lower divertor calculated from IR camera data



Downward VDE Strikes Inner Wall and Divertor Shelf

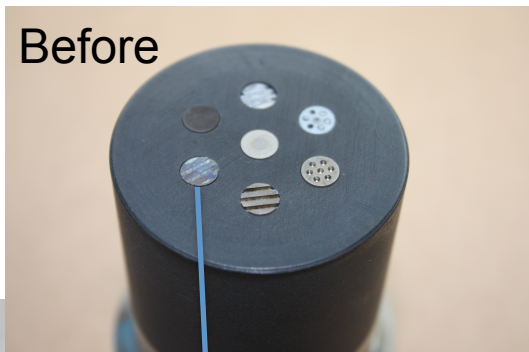
- Initial target plasma shape is standard “ITER-like” low-triangularity lower single null “LSN”
- As plasma drifts down, divertor strike points disappear and plasma limits on inner wall and limits lower divertor shelf
 - Disruption strike point broadening not well defined for VDE disruption!

JFIT reconstructions of magnetic flux surfaces during unmitigated VDE

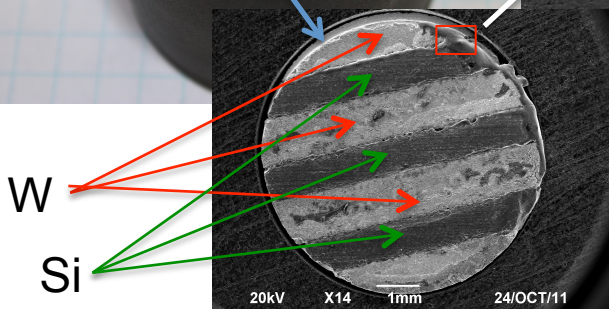
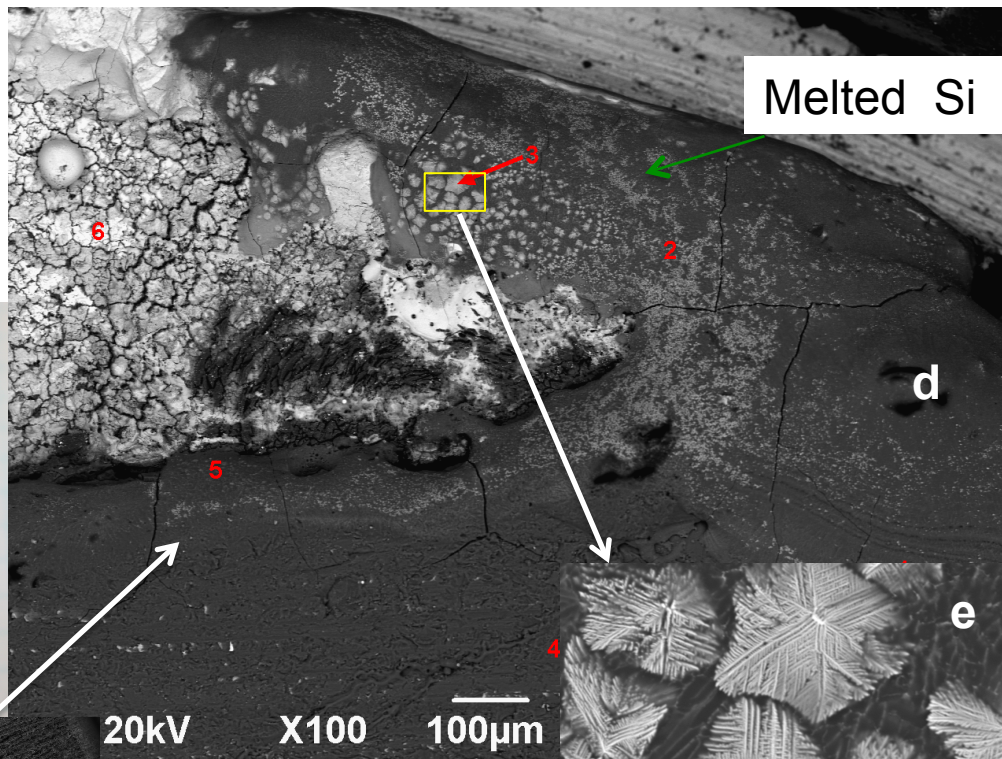
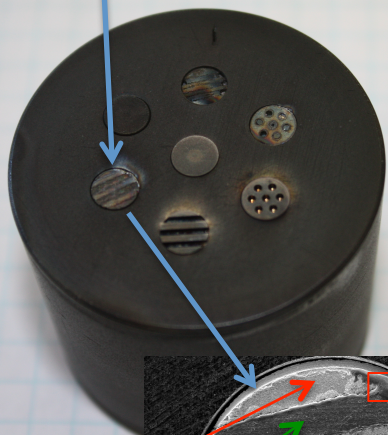


Six VDE Exposures Indicating Formation of Si-W Eutectic Mixture

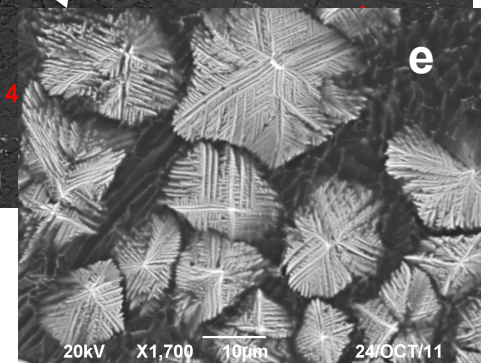
Before



After



Si MT @ 1412° C



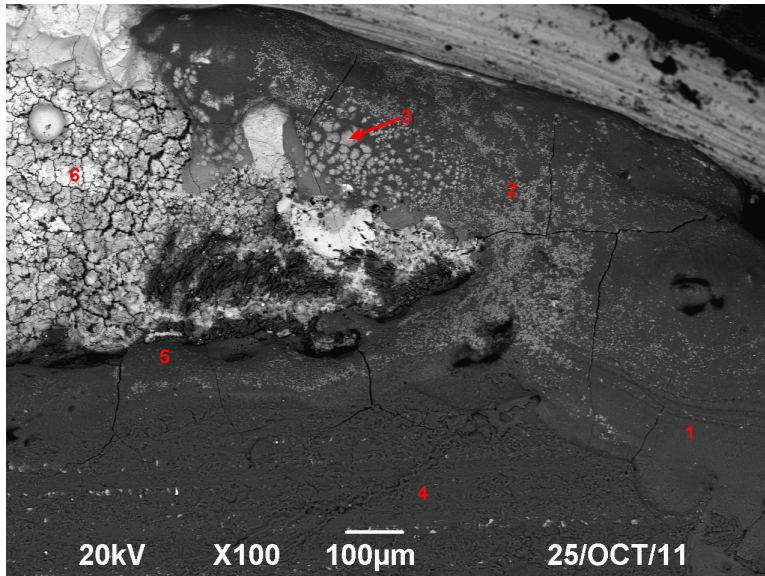
EDX views area 3

The W button with Si filled slots is damaged
The W button with empty slots is perfectly O.K.

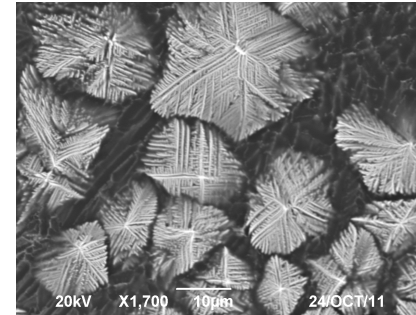
SEM and EDX Analysis at Different Locations Showing Composition of the Si-W Button at Different Areas

Spectrum	C	N	O	Al	Si	W	Total
DiMES area 1	14.24				86.35	0.0	100
DiMES area 2	21.45			0.38	69.56	8.61	100
DiMES area 3	9.57				49.31	41.11	100
DiMES area 4	32.31		13.59	0.58	53.52		100
DiMES area 5	27.10		3.01	1.99	68.00	0.0	100
DiMES area 6	20.57	7.98	19.77	4.99	7.05	39.63	100
DiMES area 7	33.97		7.75			58.28	100
DiMES area 8	46.21		5.43		12.05	36.31	100
Max.	46.21	7.98	19.77	4.99	86.35	58.28	
Min.	9.57	7.98	3.01	0.38	7.05	0.0	

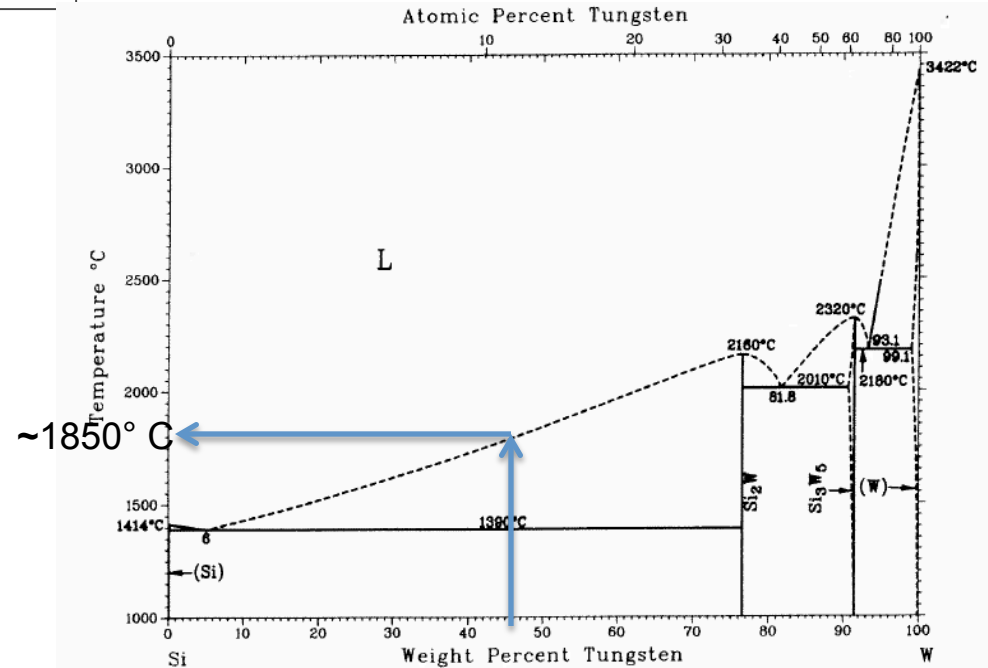
All results in wt%.



Melted Si spilled over W



SEM views area 3, W-Si crystal



S.V. Nagender Naidu, A.M. Sriramamurthy, and P. Rama Rao, 1989.

Conclusions

- Solid W is the preferred PFM; unfortunately it melts under type-I ELMs and disruption events.
- Sets of Si-W test buttons were fabricated and exposed in the DIII-D lower divertor with the goal of demonstrating the possibility of transient tolerant material design under disruption.
- During fabrication when $T \sim 1400^\circ\text{C}$, several samples were destroyed and broken into pieces.
- Si-W buttons with indentations and slots were exposed to six VDE disruptions in DIII-D and showed that part of the W surface was damaged.
- SEM photos showed tungsten-silicide crystalline structure and EDX shows composition of ~ 49.31 wt% Si and ~ 41.11 wt% W. This Si-W mixture melts at $\sim 1850^\circ\text{C}$ during a VDE disruption.
- This indicates that the Si-W combination cannot be used as a transient-tolerant surface material, since the surface temperature will be $\gg 1850^\circ\text{C}$ under a disruption event.
- This also implies that for a tokamak, to avoid surface melting, we will need to avoid type-I ELMs and disruptions to avoid melting of any metallic surface
- When Si or B is to be used as the wall conditioning material to mitigate W migration into the plasma core, in order to avoid Si-W and B-W eutectic formation, surface temperature should be lower than the lower eutectic temperature, i.e. $1410^\circ\text{C} - 100^\circ\text{C} = 1310^\circ\text{C}$ and $1970^\circ\text{C} - 100^\circ\text{C} = 1870^\circ\text{C}$, respectively.